DRAWING	SCALE:	

DRAWING SHOWN: \_\_\_\_\_

	SPECIFI curren for Ro All refe AASHT(	CATION t edition ad and erences ) LRF[	NS: Al on of d Bride s to t ) Bric	lrefe the Ke ge Cor he AAS lge Do	erence entuck hstruc SHTO S esign	;s y ;t P
	DESIGN DESIGN Bridge to 3'-0	LOADS: LOAD D Design " with	Beam ISTRIB Speci a 9" wi	n & Sla UTION: ficatia ide ba	ob sec Beam ons fo rrier.	;t s r
	FUTURE N Ioad.	WEARING	SURFAC	CE: The	ese bea	nc
	SUBSTRU DC (ki DW (k LL+I (	JCTURE ps): Be ips): F kips):	DESIGN am, Sla <sup>-</sup> uture LL wi <sup>,</sup>	N LOAD b, Diapl wear th Dyn	S: Un <sup>.</sup> hragms, ing su iamic l	fc , r
	MATERIA for for for	L DESI Beam Steel Class	GN SPE Steel Reinf "AA"	CIFICA forceme Deck (	ATIONS: ent Concre	<b>:</b> †e
	MATERIA High St Structu Shear S Sheet I	L STEE rength ural St Stud Co ead ar	L D Low eel onnect nd Pig	Alloy tors Lead		
	High st	rength	n bolts	s, nut:	s, and	,
	All steel V-Notch with the M270 GF	in lon toughn follow 50	gitudina less te ing:	al rolle st for	d wide non-fi (up t	- o
	Sampling edition, of testi	and t utilizing ng shal	esting g (H) fr I be (P).	procec equenc	lures s y test	sh in
	HIGH STR connnect washers. describe installed Specifica to the installed Put a ha	ENGTH E tions sh Open d in A with stions c chemical under ordened	BOLT CC holes ASHTO "direct and AST I requir the bo washer	ONNECTIO Shall be M164. tensio M F959. ements oft head	)NS: U 125 Gro All hig on ind All D of AS d with	nl Id Iic h IC TI TI TI
	BEVELED	EDGES:	Bevel	all exp	osed e	;d
	REINFOR( to cen center otherw bent b	CEMENT: ter o to ce ise no ars.	Dimer f bars nter oted.	nsions s unle of bar Epoxy	shown ss ot rs. Cl / coat	f h e
	CORROSI( galvani	DN PROT zed a	ECTION ccord	: Thes ing to	se bea > ASTN	m 1

DATE 5-17				5-17
<sub>BY</sub> J. Van Zee		DED	F.H.W.A.	Y <u>E. Downey</u>
DESIGNED	CHECKED	RECOMMEN	APPROVED	REVISED B

# **General Notes**

to the standard Specifications are to the Department of Highways Standard Specifications tion, with current supplemental specifications. ecifications are to the current edition of the Specifications. with interims.

ions are designed for 1.25\*HL93 (KYHL93) Live Load.

are designed according to the AASHTO LRFD beam spacings up to 6ft and overhangs up

ns are designed for a 15 PSF future wearing surface

actored design reaction forces per beam end. SIP Forms, and assumed railing dead loads of 533 lbs/ft. face.

ad allowance.

	FΥ	=	50000	ΡS
	FΥ	=	60000	ΡS
ete	F′C	=	4000	ΡS

A.S.	Т.М		A	ASH <sup>-</sup>	ГО
A709	GR	50	M270	GR	50

UNS G 1018 M-169 B29-79

washers F3125 Grade A325 M-164 Type 1

flange beams shall meet the longitudinal Charpy acture critical components Zone 2 in accordance

2" thickness) of 15 ft–1bs at 40° F.

nall be in accordance with AASHTO T243 current ng. When plate thickness exceeds  $1^{1}/_{2}^{*}$ , frequency

ess otherwise specified on the plans, all bolted de A325  $\frac{3}{4}$ " diameter high strength bolts, nuts, and ameter. Type I galvanized bolts shall be used as strength bolted field connections are to be cators" (DTI's) in accordance with the Standard 's shall be manufactured from a steel conforming M A325 for Type I galvanized steel. DTI's shall be he bumps facing the underside of the bolt head. it and tension from the nut.

dges  $\frac{3}{4}$ ".

from the face of concrete to reinforcement are nerwise shown. Spacing of bars is from ear distance to face of concrete is 2" unless all bars. Use stirrup bend diameters for all

ns and all steel components are to be hot dip A123. Weathering Steel is not allowed.

SHEAR CONNECTORS: The minimum length of stude is 6". Provide the necessary length to penetrate at least 2" above bottom of slab.

Include all costs for shear connectors with the price of the steel beams. Including shear connectors, welding and welding material, and materials necessary to field weld or shop weld the shear connectors in place according to the plans and specifications.

If the Contractor wishes to use something other than the stud shear connectors shown on the plans, the proposed arrangement shall be submitted for approval with the shop plans.

Studs shall be welded in accordance with AWS Specifications.

MILL TEST REPORTS: Notarized mill test reports shall be furnished in triplicate to the Department, showing that all material used in the structural steel conform to the requirements of the specifications.

PROHIBITED WELDING: No welding of any nature, other than indicated on the plans, is to be performed without the written consent of the designer, and then only in the manner and at the locations designated in the authorization.

SLAB: Ensure the entire superstructure slab and diaphragms are poured continuously, out to out, before allowing any concrete to set.

SHOP DRAWINGS: The fabricator shall submit all required shop plans, by email, to the design engineer for review. These submissions shall depict the shop plans in .pdf format. As either II"x17" or 22"x36" sheets. Designers will make review comments on these electronic submissions as needed and shall return them to the fabricator. Upon reconciliation of the designers comments, files shall be returned to the designer and plans will be forwarded to the Division of Structural Designs Shop Plan coordinator for distribution. Only plans submitted directly to the shop plan coordinator will be distributed and only plans electronically stamped "Distributed by The Division of Structural Design" are to be used for fabrication. While this process does not require the submission of paper copies, The Division of Structural Design reserves the right to require such copies on a case by case basis.

When any changes to the design plans are proposed by the Fabricator or Supplier, the shop drawings reflecting these changes shall be submitted to the Design Engineer through the contractor.



		TABLE O	F BEAM S	SIZES AND	DESIGN	DAT	4 (6 FT. MA)	K. BEAM	SPAC	ING WITH	I 3 FT.	MAX. O	VERHANG)
BE	AM	ROLLE	D BEAM	DEFLECTION	N IN INCHES		SHEAR CONNE	CTORS		UNFACTORED	) BEAM END	REACTION	LL DIST. FACT. (LANES)
SP	AN	BEAM MEMBER	BEAM DEPTH (IN.)	STEEL ONLY	TOTAL DL	# Per Row	Spa. @ Ea. End of Beam	Middle Spacing	ADTT	DC (kips)	DW (kips)	LL+I (kips)	LLDFM LLDFV
20′	Max.	WI8×55	8.	0.00	0.	2	10 Spa. @ 5 / <sub>4</sub> "	5¾" Spa.	300	11.85	0.90	72.65	. 877
		W 6×77	16.5	0.00	0.09	3	5 Spa. @ 5¾ "	6" Spa.	Inf.	2. 0		71.61	.865
		W   4×82	4.3	0.00	0.	3	4 Spa. @ 5¼ "	6" Spa.	450	2. 4		72.36	. 874
		W 2× 06	12.9	0.00	0.	3	4 Spa. @ 5¼ "	6" Spa.	400	12.40		71.78	.867
25′	Max.	W24×62	23.7	0.02	0.17	2	23 Spa. @ 5¼ "	6" Spa.	400	14.75	. 3	74.47	.860
		W2 ×62	21.0	0.03	0.21	2	23 Spa. @ 5¼"	6" Spa.	350	14.75		75.31	. 870
		W   8×7	18.5	0.03	0.24	2	23 Spa. @ 5¼"	6" Spa.	290	14.86		75.67	. 874
		W 6×77	16.5	0.04	0.25	3	Spa. @ 5½"	6" Spa.	Inf.	14.96		76.05	. 878
		W   4×82	4.3	0.05	0.31	3	23 Spa. @ 5 /4 "	6" Spa.	425	15.01	_	76.89	. 888
		W 2× 06	12.9	0.05	0.31	3	23 Spa. @ 51/4 "	6" Spa.	385	15.33		76.25	. 880
30′	Max.	W24×76	23.9	0.04	0.28	2	28 Spa. @ 51/4 "	6" Spa.	415	17.78	1.35	80.90	.856
		W21×83	21.4	0.05	0.32	2	28 Spa. @ 51/4 "	<u>6" Spa.</u>	350	17.89	-	81.41	. 862
		W18×86	18.4	0.06	0.39	3	(Spa. @ 5 /4 "	<u> </u>		17.94	_	82.40	• 8 ( 2
		W16×100		0.06	0.40	3	14 Spa. @ 5½"	<u>6" Spa.</u>		18.18	-	82.26	• 8 ( ]
		W14×120	4.5	0.08	0.45		28 Spa. @ 5'/4 "	6" Spa.	440	18.48	-	82.48	• 8 ( )
351	Max	$\frac{W ZX ZU}{W Z X Z U}$		0.10		ر ۲	20  Spd			18.48	1 5 9	85.41	
		W21x04	20.1	0.06	0.39	2	2/5 $0.5/4$	<u> </u>	120	20.75		86 69	. 050
		W21×101	24.5	0.07	0.47	<u>ک</u> ۲	$7 \text{ Spa}  6 \frac{1}{2}$	7" Spa	lnf	20.51	_	87 33	.052
		W18×119	19.0	0.09	0.52	3	7 Spa. @ 6"	$6^{1/2}$ " Spa.		21.43		87.50	. 860
		W   4 ×   32	4.7	0.14	0.76	3	24 Spa. @ 51/4 "	6" Spa.	425	21.66	-	89.15	.876
		W12×152	13.7	0.17	0.82	3	24 Spa. @ 5 3/8 "	6" Spa.	375	22.03	_	89.00	. 874
40′	Max.	W30×99	29.7	0.07	0.48	3	12 Spa. @ 8"	9" Spa.	lnf.	23.97	1.80	90.47	. 840
		W27×I02	27.1	0.08	0.53	3	20 Spa. @ 7½ "	9" Spa.	Inf.	24.03		91.07	. 845
		W24×117	24.3	0.09	0.56	3	14 Spa. @ 7"	8" Spa.	Inf.	24.35	-	91.22	.846
		W2 × 22	21.7	0.12	0.67	3	6 Spa. @ 6"	7" Spa.	Inf.	24.45		92.04	0.65 .854
		W 8× 30	19.3	0.15	0.81	3	9 Spa. @ 5½"	6" Spa.	Inf.	24.62		92.79	.861
		W 4× 76	15.2	0.21	0.98	3	19 Spa. @ 5¼ "	6" Spa.	425	25.58		93.11	.864
		W 2× 90	14.4	0.25	. 2	3	19 Spa. @ 5¼"	6" Spa.	375	25.86		93.25	.865
45 <i>′</i>	Ma×.	W33×118	32.9	0.09	0.54	3	12 Spa. @ 9"	IO" Spa.	Inf.	27.33	2.03	93.45	. 828
		W30×116	30.0	0.	0.64	3	21 Spa. @ 8"	IO" Spa.	Inf.	27.29	_	94.36	.836
		W27×I29	27.6	0.12	0.68	3	15 Spa. @ 7½"	9" Spa.	Inf.	27.57	_	94.53	.838
		W24×131	24.5	0. 4	0.80	3	16 Spa. @ ("	<u>8" Spa.</u>	Inf.	27.63	-	95.48	• 846
		W21×147	22.	0.17	0.91	3	17 Spa. @ 6½"	<u>("Spa.</u>		28.00	_	95.83	• 849
	Max	W18×158		0.22	1.08	3	10 Spa. @ 5½"	6" Spa.		28.25		96.54	.855
50	MAX.	W30×130		0.15	0.74	ر ۲	23 Spa $0.7$			30.60		97.11	
		W27×146	27.4	0.17	0.00	ך כו ק	18  Spa = 0.72	<u> </u>	l l n f	31.02	-	98 11	.034
		W24×162	25.0	0.20	0.05	ך <u>ר</u>	$28 \text{ Spa} = 6 \frac{1}{2}$	8" Spa	l n f	31.43	_	98.43	.030
		W2   ×   82	22.7	0.24		3	20 Spa. @ 6"	7" Spa.		31.95		98.70	. 841
		W   8 ×   92	20.4	0.30	1.36	3	$35$ Spa. @ $5\frac{1}{4}$ "	7" Spa.	lnf.	32.19	-	99.51	. 848
55′	Max.	W36×135	35.6	0.17	0.93	3	16 Spa. @ 81/4 "	10" Spa.	lnf.	33.73	2.48	100.10	. 825
		W33×141	33.3	0.18	0.99	3	25 Spa. @ 8"	10" Spa.	lnf.	33.91		100.45	. 828
		W30×148	30.7	0.21		3	28 Spa. @ 7¼ "	9" Spa.	Inf.	34.09	-	100.97	.832
		W27×178	27.8	0.23	1.10	3	19 Spa. @ 7"	8" Spa.	Inf.	34.96		100.75	.830
		W24×192	25.5	0.27	1.25	3	3  Spa. @ 6 <sup> </sup> / <sub>2</sub> "	8" Spa.	Inf.	35.33		101.20	.834
		W2 ×223	23.4	0.33	Ι.35	3	33 Spa. @ 6"	8" Spa.	lnf.	36.21		101.10	.833
		WI8×258	21.5	0.40	1.51	3	35 Spa. @ 5¾"	7" Spa.	Inf.	37.22		0 .2	.834
60′	Max.	W36×150	35.9	0.22	7	3	27 Spa. @ 8 <sup>1</sup> / <sub>4</sub> "	IO" Spa.	Inf.	37.20	2.70	102.92	. 823
		W33×169	33.8	0.24		3	18 Spa. @ 8"	9" Spa.	Inf.	37.76		102.82	. 822
		W30×173	30.4	0.27	1.32	3	30 Spa. @ 7¼ "	9" Spa.	Inf.	37.91	-	103.60	. 828
		W27×194	28.1	0.31	1.42	3	21 Spa. @ 7 "	8" Spa.	lnf.	38.56	-	103.72	. 829
		W24×229	26.0	0.37	.5	3	34 Spa. @ 6½"	8" Spa.	lnf.	39.61		103.58	.828

DATE 5-17			5-17
designed by J. Van Zee	CHECKED	RECOMMENDED	Approved F.H.w.a. Revised by <u>E. Downey</u>

DRAWING SCALE:

DRAWING SHOWN: \_\_\_\_\_

DRAWING	SCALE:	
DRAWING	SHOWN:	



DATE 5-17				2-12
designed by J. Van Zee	CHECKED	RECOMMENDED	APPROVED F.H.W.A.	revised by E. Downey

#5 F	bars (S1) placed parallel with skow		
	(5" spac. TOS & BOS)	>	
2WQII	Note: 5"Transverse Slab Reinforcemen Spacing is measured along (2 of Bridge	+ ?	2 W Q11   W Q11
Support   #1	Note: Splice S2 bars if necessary. Lap Splice 2'-5" Top of Slab Lap Splice 3'-6" Bottom of Slab	FF. Support Wall #2	& Brg. Support Wall #2 End of Bridge
bars (S2)pl 2"spa. TOS, 6 ee typical se	aced longitudinally 5" spa. BOS) ection)		
	Beam Span in Et. (© Bra. to © Bra.)	*	
011+ +0	o Out Length of Bridge (Ream Span + 2x*)	>	
			•

## PLAN OF SLAB

Note: All reinforcing steel shall be epoxy coated.

Estimate of SteelQuantities = (Bridge Length-4in)\*(Bridge Width-4in) \* (3.129 lb/sq.ft. + <u>5.006 lb/sq.ft.)</u>



Note: It is recommended a crash tested barrier be attached to the Superstructure to contain all vehicles within the roadway. Recommended barriers include the Type T631 guardrail, Type 3, or 32" Vertical Face railing. See contract documents for required railing and railing drawings for additional reinforcement that may be required to be cast in deck.





#5 Skewed Transverse Bar (S1)Length = Bridge Width - 4" SF

$$* = \frac{\frac{1}{2}Wall}{SF}$$

Skew	Factors
Skew	SF
$\bigcirc$ °	1.000
° 5	0.996
() °	0.985
° 5	0.966
20°	0.940
25°	0.906
30°	0.866
35°	0.819
40°	0.766
45°	0.707

	Skew Facto	)rs	
Skew	SF	DM	┥
0 °	1.000	0.000	
5°	0.996	0.087	
10°	0.985	0.176	_
15°	0.966	0.268	- s
20-	0. 940 0. 906	0.364	-
300	0.866	0.577	_
35°	0.819	0.700	-
40°	0.766	0.839	
45°	0.707	.000	] /
* = (O. <u>E</u>	5xBeam Spacing	ping x DM)	
	SF		
	(LAbutme	ent or	
	€ End	Bent-	
			7
			-
			Note Uso3/."
			Note: Use <sup>3</sup> /4" <sup>13</sup> /16 "Ø H
			Note: Use <sup>3</sup> /4" <sup> 3</sup> / <sub>16</sub> "Ø H
L8×4× <sup>1</sup> /2"	x7 <sup>1</sup> /2"   ong (*	$\frac{2\frac{3}{4}}{3}$	Note: Use <sup>3</sup> /4" <sup>13</sup> / <sub>16</sub> "Ø H
L8×4× <sup>1</sup> /2"	x7 <sup>1</sup> /2" Long (*	typ.)	Note: Use <sup>3</sup> /4" <sup>13</sup> / <sub>16</sub> "Ø +
L8×4× <sup>l</sup> /2"	x7 <sup>1</sup> / <sub>2</sub> " Long (- 	typ.) $2\frac{3}{4}$	Note: Use $\frac{3}{4}$ " $\frac{13}{16}$ "Ø
L8×4× <sup>1</sup> /2"	x7 <sup>1</sup> / <sub>2</sub> " Long (- Ēc l	typ.) 23/4"	Note: Use <sup>3</sup> /4" <sup>13</sup> / <sub>16</sub> "Ø t
L8×4× <sup>1</sup> /2"	x7 <sup>1</sup> / <sub>2</sub> " Long (- Ēr l	<pre> 23/4" 23/4" 23/4" 2 3/4"</pre>	Note: Use $\frac{3}{4}$ " $\frac{13}{16}$ "Ø
L8×4× <sup>1</sup> /2"	x7 <sup>1</sup> / <sub>2</sub> " Long (- īr l	typ.) $\frac{2^{3/4}}{1^{1/4}}$	Note: Use $\frac{3}{4}$ " $\frac{3}{16}$ "Ø
L8×4× <sup>1</sup> /2"	x7 <sup>1</sup> / <sub>2</sub> " Long (* īr l	typ.) $2\frac{3}{4}$	Note: Use $\frac{3}{4}$ " $\frac{3}{16}$ "Ø
L8×4× <sup>1</sup> /2"	x7 <sup>1</sup> / <sub>2</sub> " Long (* īr l	<u>23/4</u> <u>11/4</u> <u>SECTIO</u>	Note: Use $\frac{3}{4}$ " $\frac{13}{16}$ "Ø
L8×4× <sup>1</sup> /2"	x7 <sup>1</sup> / <sub>2</sub> " Long (* īr l	<u>23/4</u> <u>11/4</u> <u>SECTIO</u>	Note: Use $\frac{3}{4}$ " $\frac{13}{16}$ "Ø the second seco
L8×4× <sup>1</sup> /2"	x7 <sup>1</sup> / <sub>2</sub> " Long (* īr l	<sup>23/4</sup> <sup>1/4</sup> <b>SECTIO</b>	Note: Use $\frac{3}{4}$ " Note: Use $\frac{3}{13}$ " C7×9.8 Note: Use $\frac{3}{4}$ "
L8×4× <sup>1</sup> /2"	x7 <sup>1</sup> / <sub>2</sub> " Long (* īr l	<sup>23/4</sup> <sup>+</sup> yp.) <sup>+</sup> <sup>+</sup> <sup>+</sup> <sup>+</sup> <sup>+</sup> <sup>+</sup> <sup>+</sup> <sup>+</sup>	Note: Use $\frac{3}{4}$ " Note: Use $\frac{3}{6}$ " Note: Use $\frac{3}{6}$ " Note: Use $\frac{3}{4}$ " Note: Use $\frac{3}{6}$ "
L8×4× <sup>1</sup> /2"	x7 <sup>1</sup> / <sub>2</sub> " Long (* Ēr l	2 <sup>3</sup> / <sub>4</sub> " = 1 <sup>1</sup> / <sub>4</sub> " SECTIO	Note: Use $\frac{3}{4}$ " Note: $\frac{3}{13}$ " Note: Use $\frac{3}{4}$ " Note: Use $\frac{3}{4}$ " Note: Use $\frac{3}{4}$ "
L8×4× <sup>1</sup> / <sub>2</sub> "	×7 <sup>1</sup> /2" Long (٦ لا ۱۵، ۱۰۰ ۱۰۰ ۱۰۰ ۱۰۰ ۱۰۰ ۱۰۰ ۱۰۰ ۱۰۰ ۱۰۰ ۱۰	SECTION 5 5 5 5 5 5 5 7 1 1 4 1 4 5 5 7 1 1 4 5 7 1 1 4 1 1 4 1 1 4 1 1 4 1 1 1 1 1 1 1 1 1 1 1 1 1	Note: Use $\frac{3}{4}$ " Note: $\frac{5}{13}$ $\frac{1}{6}$ "Ø" $C7 \times 9.8$ <b>DN A-A</b> Note: Use $\frac{3}{4}$ " $\frac{1}{3}$ $\frac{1}{6}$ "Ø"
L8×4× <sup>1</sup> / <sub>2</sub> "	×7 <sup>1</sup> / <sub>2</sub> " Long (	$\frac{2^{3/4}}{1^{1/4}}$	Note: Use $\frac{3}{4}$ Note: Use $\frac{3}{4}$ C7×9.8 <b>DN A-A</b>
L8×4× <sup>1</sup> /2"	×7 <sup>1</sup> / <sub>2</sub> " Long (- لا ×10 <sup>1</sup> / <sub>2</sub> " Long (-	typ.) typ.) SECTION	Note: Use $\frac{3}{4}$ Note: Use $\frac{3}{4}$ $\frac{1}{3}$ $\frac{1}{6}$ $\frac{1}{9}$ $\frac{1}{9}$ $\frac{1}{9}$ $\frac{1}{9}$ Note: Use $\frac{3}{4}$ $\frac{1}{3}$ $\frac{1}{6}$ $\frac{1}{9}$
L8×4× <sup>1</sup> /2"	x7 <sup>1</sup> / <sub>2</sub> " Long (	$\frac{2^{3/4}}{1^{1/4}}$	Note: Use $\frac{3}{4}$ Note: Use $\frac{3}{6}$ C7x9.8 <b>DN A-A</b> Note: Use $\frac{3}{4}$ Note: Use $\frac{3}{4}$ $\frac{1}{3}$ $\frac{1}{6}$ $\frac{1}{9}$
$L8 \times 4 \times \frac{1}{2}$	x7 <sup>1</sup> / <sub>2</sub> " Long (* [] x10 <sup>1</sup> / <sub>2</sub> " Long (*	Typ.)	Note: Use $\frac{3}{4}$ Note: Use $\frac{3}{6}$ $C7 \times 9.8$ <b>DN A-A</b> Note: Use $\frac{3}{4}$ $\frac{1}{3}/6$ "Ø
L8×4× <sup>1</sup> /2"	x7 <sup>1</sup> / <sub>2</sub> " Long ( 	$\frac{2^{3/4}}{\sqrt{2^{3/4}}}$	Note: Use $\frac{3}{4}$ ", $\frac{3}{6}$ ", $\frac{1}{9}$ ", $\frac{1}{13}$ , $\frac{1}{6}$ ", $\frac{1}{9}$ ", $\frac{1}{13}$ , $\frac{1}{6}$ ", $\frac{1}{9}$ ", $\frac{1}{13}$ , $\frac{1}{6}$ ", $\frac{1}{9}$ ", $\frac{1}{13}$ , $\frac{1}{13}$ , $\frac{1}{13$
$\lfloor 8 \times 4 \times \frac{1}{2} \end{bmatrix}$	x7 <sup>1</sup> / <sub>2</sub> " Long (* [ x10 <sup>1</sup> / <sub>2</sub> " Long (*	$\frac{2\sqrt[3]{4}}{\sqrt{1/4}}$	Note: Use $\frac{3}{4}$ $\frac{1}{3}$ $\frac{1}{6}$ $\frac{1}{9}$ $\frac{1}{3}$ $\frac{1}{6}$ $\frac{1}{3}$ $\frac{1}{6}$ $\frac{1}{3}$ $\frac{1}{6}$ $\frac{1}{3}$ $\frac{1}{6}$ $\frac{1}{3}$ $\frac{1}{6}$ $\frac{1}{9}$ $\frac{1}{3}$ $\frac{1}{6}$ $\frac{1}{3}$ $\frac{1}{6}$ $\frac{1}{3}$ $\frac{1}{6}$ $\frac{1}{3}$ $\frac{1}{6}$ $\frac{1}{3}$ $\frac{1}{6}$ $\frac{1}{3}$ $\frac{1}{6}$ $\frac{1}{3}$ $\frac{1}{6}$ $\frac{1}{3}$
L8×4× <sup>1</sup> / <sub>2</sub> "	x7 <sup>1</sup> / <sub>2</sub> " Long (* k10 <sup>1</sup> / <sub>2</sub> " Long (*	$\frac{2^{3/4}}{1^{4/4}}$	Note: Use $\frac{3}{4}$ " Note: Use $\frac{3}{2}$ " Note: Use $\frac{3}{4}$ "
L8×4×1/2"	x7 <sup>1</sup> / <sub>2</sub> " Long (* 10 <sup>1</sup> / <sub>2</sub> " Long (*	SECTION SEC	Note: Use $\frac{3}{4}$ Note: Use $\frac{3}{7}$ $\sqrt{2}$
L8×4× <sup>1</sup> / <sub>2</sub> "	x7 <sup>1</sup> / <sub>2</sub> " Long ( x10 <sup>1</sup> / <sub>2</sub> " Long (-	$\frac{2^{3/4}}{\sqrt{1/4}}$	Note: Use $\frac{3}{4}$ Note: $\frac{3}{16}$ $\frac{5}{6}$ $\frac{5}$

RAWING	SCALE:
DRAWING	SHOWN:

DATE 5-17				5-17
designed by J. Van Zee	CHECKED	RECOMMENDED	APPROVED F.H.W.A.	REVISED BY E. DOWNEY





рате 5-17				2-17
designed by J. Van Zee	CHECKED	RECOMMENDED	APPROVED F.H.W.A.	revised by <u>E. Downey</u>

 $L8 \times 4 \times \frac{1}{2}$ "×1′-6" Long —

123/4" @4<sup>|</sup>/4"

DRAWING SCALE: \_\_\_\_\_

DRAWING SHOWN: \_\_\_\_\_



DEPARTMENT OF HIGHWAYS COMPOSITE STEEL BEAM SUPERSTRUCTURES

DIAPHRAGMS CONTINUED

STANDARD DRAWING NO. BDE-001-01

SUBMITTED Mark Auto STATE HIGHWAY ENGINEE APPROVE

12-02-11 DATE 12-02-11 DATE

KENTUCKY

DRAWING	SCALE:	

DRAWING SHOWN: \_\_\_\_\_



DATE 5-17				5-17
Jesigned By J. Van Zee	CHECKED	RECOMMENDED	APPROVED F.H.W.A.	REVISED BY E. DOWNEY

Mastic Tape shall cover the joint continuously unless otherwise shown in the plans. Mastic Tape shall be spliced by lapping a minimum of six inches and in accordance with the mfgrs. recommendations with the overlap running

The cost of labor, materials, and incidental items for furnishing and installing Mastic Tape shall be considered incidental to the unit price bid for Concrete Class 'AA' and no separate measurement or payment shall be made.

